

# Fe-Ni-Ti (Iron-Nickel-Titanium)

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The review of this system by [1990Gup] pertained mainly to the experimental studies of [1938Vog], [1967Dud] and [1981Loo] and presented a partial liquidus projection for the Ti-lean region, a full isothermal section at 900 °C, partial isothermal sections at 1100, 1027 and 700 °C and four vertical sections at 12 mass% Ti, at Fe:Ni mass ratio 90:10 and 40:60 and along the FeTi-NiTi join respectively. An update by [2001Gup] reviewed the experimental results of [1994Ali], who determined a partial liquidus projection and several vertical sections in the Ti-rich region. Recently, the phase equilibria in Ti-rich alloys were studied by [2006Ria], who presented a partial isothermal section at 900 °C for Ti-rich alloys and a vertical section at 66 at.% Ti. From the same group of workers, [2006Cac] presented a critical evaluation of the system and presented for the entire composition range a liquidus projection, isothermal sections at 1000 °C [1999Abr] and 900 °C [1981Loo] and several vertical sections. Very recently, [2009Key] carried out a thermodynamic assessment of the system, as a sequel to the review by [2006Cac].

## Binary Systems

The Fe-Ni phase diagram [1991Swa] is characterized by a very narrow solidification range with a peritectic reaction at 1514 °C, between bcc  $\delta$  (or  $\alpha$ ) and liquid that yields the Fe-based fcc solid solution. A continuous fcc solid solution

denoted  $\gamma$  is stable over a wide range of temperature. At 517 °C, an ordered phase  $\text{FeNi}_3$  ( $L1_2$ , AuCu<sub>3</sub>-type cubic) forms congruently from  $\gamma$ . At 345 °C,  $\gamma$  decomposes to ( $\alpha + \text{FeNi}_3$ ). The Fe-Ti phase diagram [1998Dum] depicts two intermediate phases:  $\text{Fe}_2\text{Ti}$  ( $C14$ , MgZn<sub>2</sub>-type hexagonal) and  $\text{FeTi}$  ( $B2$ , CsCl-type cubic). The computed Fe-Ti phase diagram of [2009Key] shows a smaller homogeneity range of  $\text{Fe}_2\text{Ti}$  (especially at lower temperatures) than that indicated in earlier reports. The Ni-Ti phase diagram [2009Key] has three intermediate phases:  $\text{Ni}_3\text{Ti}$  ( $DO_{24}$ , Ni<sub>3</sub>Ti-type hexagonal),  $\text{NiTi}$  ( $B2$ , CsCl-type cubic) and  $\text{NiTi}_2$  ( $E9_3$ -type cubic).

## Computed Ternary Phase Equilibria

The liquid and the disordered part of the solid solutions (bcc, fcc and cph) were described as substitutional solutions by [2009Key]. To be applicable in a future modeling of the Al-Fe-Ni-Ti quaternary system, a four sublattice model was used for the ordered fcc phases. An ordering energy term was added to the Gibbs energy term describing the disordering state. The intermetallic phases such as  $\text{NiTi}_2$ ,  $\text{NiTi}$ ,  $\text{Ni}_3\text{Ti}$ ,  $\text{FeTi}$  and  $\text{Fe}_2\text{Ti}$  were modeled with two or more sublattices with provision for the ternary solubility, which is appreciable in these phases. The optimized parameters for all the phases were listed.

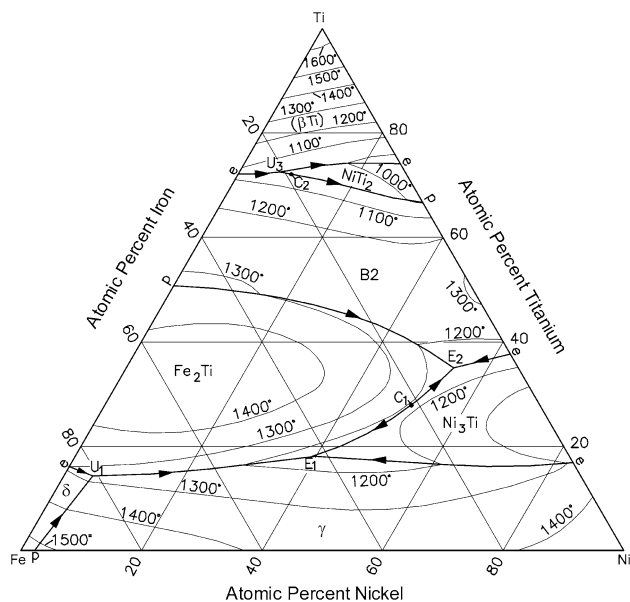


Fig. 1 Fe-Ni-Ti computed liquidus projection [2009Key]

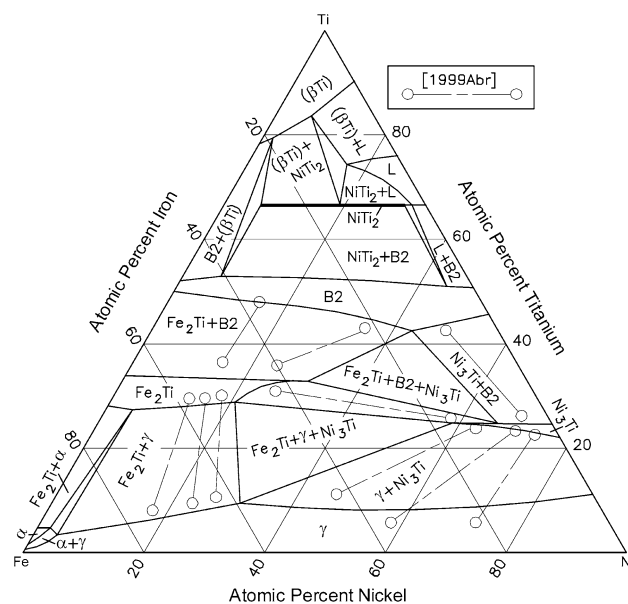
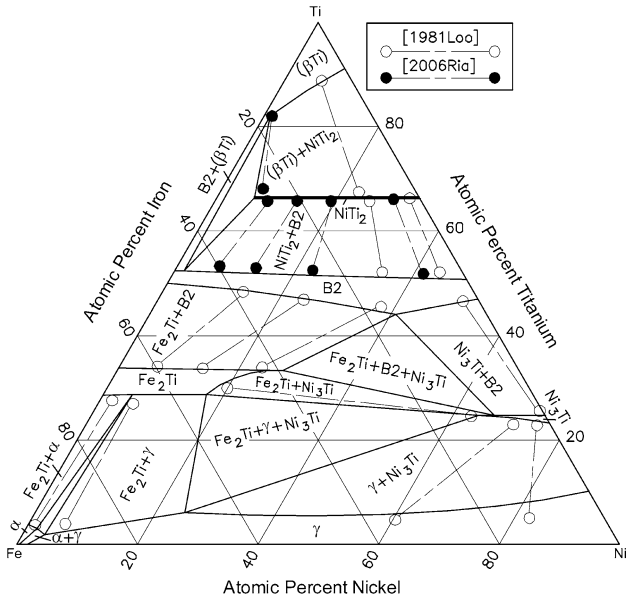


Fig. 2 Fe-Ni-Ti computed isothermal section at 1000 °C [2009Key]

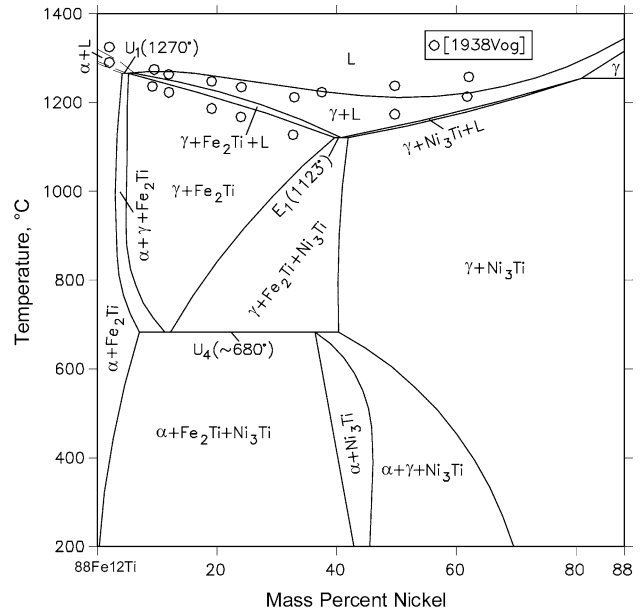
[2009Key] computed a liquidus projection, five isothermal sections at 1300, 1000, 900, 600 and 100 °C, and four vertical sections at 66 at.% Ti, 12 mass% Ti, Fe/Ni atom ratio = 1 and Fe/Ni mass ratio = 4/6, respectively. The calculated sections were compared with the available experimental data from the literature. No experimental data are known for comparison with the isothermal sections

computed at 600 and 100 °C. Two metastable isothermal sections at 700 °C depicting the equilibria between the ordered and disordered forms of bcc and fcc respectively were also computed by [2009Key].

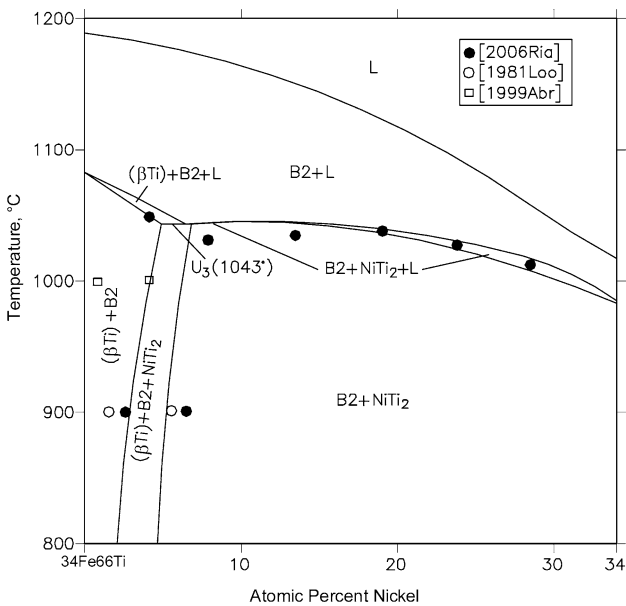
The computed liquidus projection is shown in Fig. 1. The monovariant liquidus lines in Fig. 1 generally agree with those evaluated by [2006Cac]. At the Ti-lean region, the



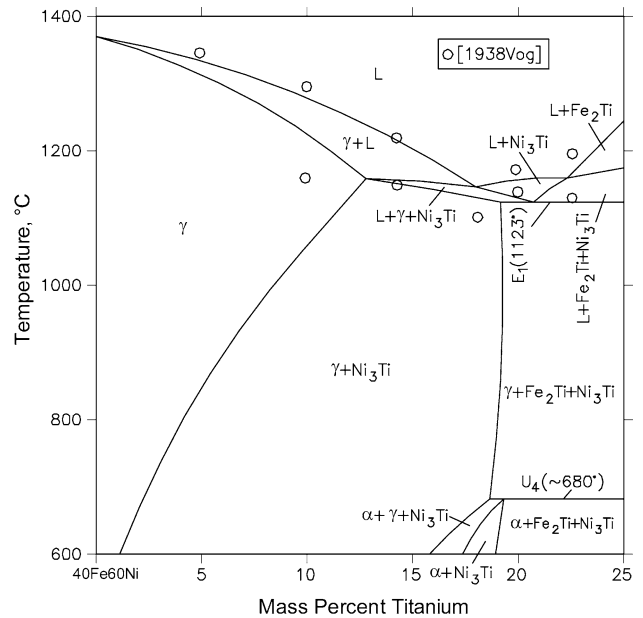
**Fig. 3** Fe-Ni-Ti computed isothermal section at 900 °C [2009Key]



**Fig. 5** Fe-Ni-Ti computed vertical section at 12 mass% Ti [2009Key]



**Fig. 4** Fe-Ni-Ti computed vertical section at 66 at.% Ti [2009Key]



**Fig. 6** Fe-Ni-Ti computed vertical section at Fe/Ni mass ratio of 4/6 [2009Key]

## Section II: Phase Diagram Evaluations

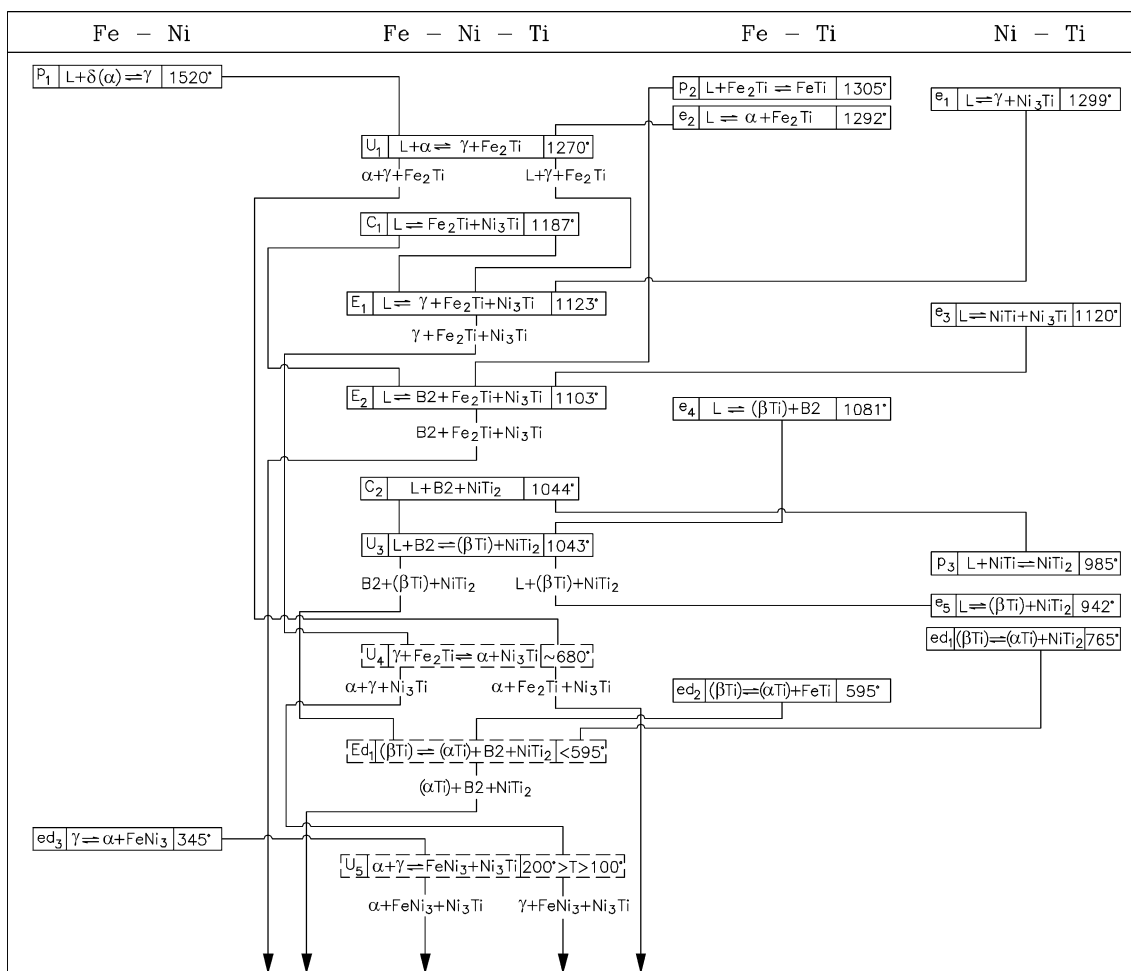


Fig. 7 Fe-Ni-Ti reaction sequence [after 2009Key]

final solidification occurs through two ternary eutectic reactions  $E_1$  and  $E_2$ .  $NiTi_2$  nucleates in the ternary region at the critical point  $C_2$  [2009Key].  $C_2$  is very close to the transition reaction  $U_3$  (just 1 °C higher).

The isothermal section computed by [2009Key] at 1300 °C was compared with the experimental results of [1982Dra] in the Ti-lean region. This section is not consistent with the liquidus projection and the reaction scheme given by [2009Key]. The reasons for this anomaly are not clear. The computed isothermal sections at 1000 and 900 °C are shown in Fig. 2 and 3. The agreement with the experimental data is generally good. The isomorphous pair FeTi-NiTi forms a continuous solid solution  $B2$  at all temperatures from 1300 to 100 °C.

Three computed vertical sections at 66 at.% Ti, 12 mass% Ti and Fe/Ni mass ratio = 4/6 respectively are shown in Fig. 4-6. The reactions at the invariant horizontal are indicated. The agreement with the experimental data is satisfactory. A reaction sequence written by [2009Key] is shown in Fig. 7. Using the computed isothermal sections at 600 and 100 °C and the vertical sections of [2009Key] as a guide, the reaction sequence has been extended down to room temperature.

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